

Resonantly induced friction in driven nanomechanical systems

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We propose a new mechanism of friction in resonantly driven vibrational systems. The form of the friction force follows from the time- and spatial-symmetry arguments. We consider a microscopic mechanism of this resonant force in nanomechanical systems. The friction can be negative, leading to an instability of forced vibrations of a nanoresonator and the onset of self-sustained oscillations in the rotating frame.

The physics of friction keeps attracting attention in diverse fields and at different spatial scales, from cold atoms to electrons on helium to locomotion of devices and animals [1–5]. An important type of systems where friction plays a critical role and where it has been studied in depth, both theoretically and experimentally, are vibrational systems. The simplest form of friction in these (and many other) systems is viscous friction. For a vibrational mode with coordinate q , the viscous friction force is $\propto \dot{q}$. It describes a large number of experiments on various kinds of vibrational systems, nano- and micro-mechanical modes and electromagnetic cavity modes being examples of the particular recent interest [6, 7].

In vibrational systems, viscous friction is often called linear friction, to distinguish it from nonlinear friction, which nonlinearly depends on q and \dot{q} . Phenomenologically, the simplest nonlinear friction force is $\propto q^2\dot{q}$ (the van der Pol form [8]) or $\propto \dot{q}^3$ (the Rayleigh form [9]). Both these forms of the force are particularly important for weakly damped systems. This is because in such systems the vibrations are nearly sinusoidal, whereas both forces have resonant components which oscillate at the mode frequency. Moreover, both forces lead to the same long-term dynamics of a weakly damped mode and in this sense are indistinguishable [10, 11].

External driving of vibrational modes can modify their dissipation. The change has been well understood for a periodic driving tuned sufficiently far away from the mode eigenfrequency. Such driving can open new decay channels where transitions between the energy levels of the mode are accompanied by absorption or emission of excitations of the thermal reservoir and a drive quantum $\hbar\omega_F$, with ω_F being the drive frequency [12]. This can lead to both linear [13, 14] and nonlinear friction [15, 16]. It has been also found that, in microwave cavities and nanomechanical systems, resonant driving can reduce linear friction by slowing down energy transfer from the vibrational mode to two-level systems due to their saturation [17–19].

In this paper we consider nonlinear friction induced by resonant driving, which significantly differs from other forms of friction. We show that, in nanomechanical systems, the proposed friction can become important already for a moderately strong drive and can radically

modify the response to the drive, including the onset of slow oscillations of the amplitude and phase of the driven mode with the increasing drive [20].

Phenomenologically, a mode with inversion symmetry driven by a force $F(t) = F \cos \omega_F t$ can experience a resonant induced friction force (RIFF) of the form

$$f_{\text{RIFF}} = \eta_{\text{RIFF}} F(t) q \dot{q}. \quad (1)$$

Such force has the right spatial symmetry, as it changes sign on spatial inversion ($q \rightarrow -q$ and $F \rightarrow -F$), and is dissipative, as it changes sign on time inversion $t \rightarrow -t$. The driving frequency ω_F is assumed to be close to the mode eigenfrequency ω_0 , so that the force f_{RIFF} has a resonant component. Parameter η_{RIFF} is the friction coefficient, which is undetermined in the phenomenological theory. Not only the magnitude, but also the sign of η_{RIFF} are not determined, as the very onset of the force f_{RIFF} is a nonequilibrium phenomenon.

The form of the RIFF reminds the form of the van der Pol friction force, except that q^2 is replaced by $F(t)q$. In some sense, the force $F(t)$ is “smaller” than the displacement q near resonance: this is the well-known effect that a small resonant force leads to large vibration amplitude for weak damping. Therefore f_{RIFF} can be significant if there is a mechanism that compensates the relative smallness of $F(t)$.

For nanomechanical resonators, a simple microscopic mechanism of the RIFF is heating. The absorbed power $F(t)\dot{q}$ leads to a temperature change δT , which can be relatively large due to the small thermal capacity of a nanoresonator [generally, the temperature change depends on the coordinates in the resonator, see Appendix]. In turn, the temperature change modifies the resonator eigenfrequency ω_0 , for example, due to thermal expansion, cf. [21, 22]. To the lowest order in δT , the eigenfrequency change is $\delta\omega_0 = -\lambda_\omega \delta T$ with the coefficient λ_ω depending on the spatial structure of the mode and the temperature field.

In many cases, the relaxation time of the temperature in the resonator is much longer than the vibration period $t_F = 2\pi/\omega_F$. Then the temperature change is proportional to the period-averaged power,

$$\delta T(t) = \lambda_T [F(t)\dot{q}(t)]_{\text{av}} \equiv \lambda_T t_F^{-1} \int_t^{t+t_F} dt' F(t') \dot{q}(t')$$

(in fact, δT is spatially nonuniform, see Appendix). As a result, the restoring force $-m\omega_0^2 q$ is incremented by f_T ,

$$f_T(t) = 2m\omega_0\lambda_\omega\lambda_T[F(t)\dot{q}(t)]_{\text{av}} q(t) \quad (2)$$

The force $f_T(t)$ is a specific form of the RIFF. The thermal mechanism is not the only RIFF mechanism, but it is often important, and moreover, the ratio of the conventional nonlinear friction to the RIFF contains a small parameter, see Appendix.

We now consider the dynamics of a driven nanoresonator in the presence of RIFF. Nanoresonators are often well described by the Duffing model, which takes into account a quartic nonlinearity [10]. The Hamiltonian of the Duffing oscillator in the absence of coupling to the thermal reservoir is

$$H_0 = \frac{1}{2}(p^2 + \omega_0^2 q^2) + \frac{1}{4}\gamma q^4 - qF \cos \omega_F t. \quad (3)$$

Here p is the oscillator momentum. We have set the mass $m = 1$. For concreteness, we assume that the Duffing nonlinearity parameter γ is positive. The driving is assumed resonant, $|\omega_F - \omega_0| \ll \omega_0$, and comparatively weak, so that $|\gamma|\langle q^2 \rangle \ll \omega_0^2$.

To analyze the behavior on the time scale long compared to ω_F^{-1} , one can change to the rotating frame and introduce slowly varying in time canonically conjugate coordinate q_0 and momentum p_0 (the analogs of the quadrature operators)

$$q(t) + i\omega_F^{-1}p(t) = (\omega_F)^{-1/2}(q_0 + ip_0) \exp(-i\omega_F t).$$

In the standard rotating wave approximation (RWA), from Eq. (3) we obtain Hamiltonian equations for q_0, p_0 with the time-independent Hamiltonian H_{RWA} ,

$$\begin{aligned} (\dot{q}_0)_H &= \partial_{p_0} H_{\text{RWA}}, & (\dot{p}_0)_H &= -\partial_{q_0} H_{\text{RWA}}, \\ H_{\text{RWA}}(q_0, p_0) &= -\frac{1}{2}\delta\omega(q_0^2 + p_0^2) + \frac{3\gamma}{32\omega_F^2}(q_0^2 + p_0^2)^2 \\ &- Fq_0/2\sqrt{\omega_F}, & \delta\omega &= \omega_F - \omega_0. \end{aligned} \quad (4)$$

It is well-known how to incorporate linear friction into the RWA-equations of motion starting from both a microscopic formulation and the phenomenological friction force $-2\Gamma\dot{q}$ [23–26]. An extension to the RIFF is straightforward. Keeping only smoothly varying terms in the equations for \dot{q}_0, \dot{p}_0 , in the case of the heating-induced RIFF (2) we obtain the following equations of motion:

$$\begin{aligned} \dot{q}_0 &= -\Gamma q_0 - J_T p_0^2 + \partial_{p_0} H_{\text{RWA}}, \\ \dot{p}_0 &= -\Gamma p_0 + J_T q_0 p_0 - \partial_{q_0} H_{\text{RWA}}. \end{aligned} \quad (5)$$

Here $J_T = \omega_F^{1/2} F \lambda_\omega \lambda_T / 2$. In Eq. (5) we have disregarded noise. It is typically weak in weakly damped nanoresonators and leads primarily to small fluctuations about the stable states of forced vibrations and occasional switching between the stable states in the range of bistability, cf. [26–32] and references therein; here we do not consider these effects.

The parameter J_T that characterizes the RIFF increases with the driving amplitude F ; the RIFF also increases with the vibration amplitude $A = [(q_0^2 + p_0^2)/\omega_F]^{1/2}$. From Eq. (5), the effects of the RIFF become pronounced for $|J_T A| \sim \Gamma$ and should be seen already for a moderately strong drive if the decay rate Γ due to the linear friction is small.

If the linear friction and the RIFF can be disregarded, the values $(q_{\text{st}}, p_{\text{st}})$ of (q_0, p_0) at the stationary states of forced vibrations are given by the conditions $\partial_{q_0} H_{\text{RWA}} = \partial_{p_0} H_{\text{RWA}} = 0$, which reduce to equations

$$\frac{3\gamma}{8\omega_F^2} q_{\text{st}}^3 - \delta\omega q_{\text{st}} = F/2\sqrt{\omega_F}, \quad p_{\text{st}} = 0. \quad (6)$$

The equation for q_{st} has one real root in the range of $F, \delta\omega$ where the oscillator is monostable in the weak dissipation limit or 3 real roots in the range of bistability. In the latter range, of primary interest for the analysis of the RIFF is the root with the maximal q_{st} , and in what follows q_{st} refers to this root. For small Γ and $J_T = 0$ it corresponds to a stable state of forced vibrations at frequency ω_F , as does also the real root q_{st} in the range of monostability [33]. In the both cases, the considered $(q_{\text{st}}, p_{\text{st}})$ corresponds to the minimum of H_{RWA} .

For $J_T > 0$ the RIFF can lead to instability of the forced vibrations. Indeed, to the leading order in Γ, J_T , the sum of the eigenvalues of Eqs. (5) linearized about the stable state is $-2\Gamma + J_T q_{\text{st}}$. When this sum becomes equal to zero, the system undergoes a supercritical Hopf bifurcation. This means that, for $J_T q_{\text{st}} > 2\Gamma$, the state of forced vibrations with constant amplitude and phase becomes unstable. The amplitude and phase oscillate in time, which corresponds to oscillations of the system in the rotating frame about $(q_{\text{st}}, p_{\text{st}})$.

For small Γ and $J_T q_{\text{st}}$ (the condition is specified below), one can think of the steady motion in the rotating frame as occurring with a constant value of the Hamiltonian H_{RWA} along the Hamiltonian trajectory (4), see Fig. 1(a). This value is determined by the balance of the damping $\propto \Gamma$ and the RIFF. The dissipative losses $\propto \Gamma$ drive H_{RWA} toward its minimum, whereas the RIFF pumping increases H_{RWA} . The stationary value of H_{RWA} can be found by averaging over the trajectories (4) the equation of motion for $H_{\text{RWA}}(q_0, p_0)$, which follows from Eq. (5). We denote such averaging by an overline,

$$\overline{U(t)} = \frac{1}{\mathbb{T}(H_{\text{RWA}})} \int_t^{t+\mathbb{T}(H_{\text{RWA}})} dt' U(t'; H_{\text{RWA}}),$$

where $U(t; H_{\text{RWA}})$ is a function calculated along the trajectory (4) for a given value of H_{RWA} and $\mathbb{T}(H_{\text{RWA}})$ is the period of motion along this trajectory. After straightforward algebra we obtain from Eqs. (5)

$$\begin{aligned} \overline{dH_{\text{RWA}}/dt} &= \frac{1}{\mathbb{T}(H_{\text{RWA}})} \int_{\mathcal{S}(H_{\text{RWA}})} dq_0 dp_0 (-2\Gamma + J_T q_0). \end{aligned} \quad (7)$$

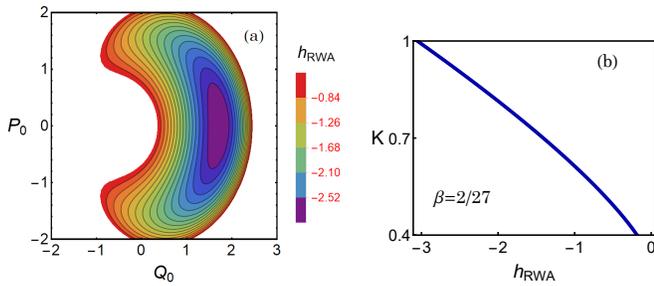


FIG. 1. (a) The Hamiltonian trajectories (4) for different values of $h_{\text{RWA}} \propto H_{\text{RWA}}$ and the scaled field strength $\beta = 2/27$. The driven oscillator is bistable for this β , and shown are the trajectories that circle the large-amplitude state at the minimum of h_{RWA} , which is stable in the absence of RIFF. The trajectories have a horse-shoe form away from the minimum of h_{RWA} also where the oscillator is monostable. (b) The scaled ratio of the relaxation rates K , Eq. (8), as a function of the scaled RWA energy $h \propto H_{\text{RWA}}$, Eq. (9).

Here, $\mathcal{S}(H_{\text{RWA}})$ is the area inside the Hamiltonian trajectory (4) with a given H_{RWA} .

From Eq. (7), the stationary (and stable) value of H_{RWA} is determined by equation

$$(J_T q_{\text{st}}/2\Gamma) K = 1,$$

$$K = q_{\text{st}}^{-1} \int_{\mathcal{S}(H_{\text{RWA}})} q_0 dq_0 dp_0 \left[\int_{\mathcal{S}(H_{\text{RWA}})} dq_0 dp_0 \right]^{-1}. \quad (8)$$

Parameter K gives the ratio of the relaxation rates due to the RIFF and the linear friction. It is the dependence of K on H_{RWA} that allows one to find the stable value of H_{RWA} from Eq. (8). This dependence is illustrated in Fig. 1(b).

Figure 1 is plotted in the scaled variables Q_0, P_0 and for the scaled Hamiltonian $h_{\text{RWA}} = (6\gamma/F^4)^{1/3} H_{\text{RWA}}$,

$$h_{\text{RWA}} = \frac{1}{4}(Q_0^2 + P_0^2)^2 - \frac{1}{2}\beta^{-1/3}(Q_0^2 + P_0^2) - Q_0, \\ Q_0 = q_0/\zeta, P_0 = p_0/\zeta, \quad \zeta = (4F/3\gamma)^{1/3}\omega_F^{1/2}. \quad (9)$$

Function h_{RWA} depends only on one dimensionless parameter, the scaled strength of the driving field

$$\beta = 3\gamma F^2/32\omega_F^3(\delta\omega)^3.$$

As seen from Fig. 1(b) and also from Eq. (9), $K = 1$ where $h \propto H_{\text{RWA}}$ is at its minimum. Importantly, K monotonically decreases with increasing H_{RWA} in a broad range of H_{RWA} . This decrease holds both in the range of β where the oscillator is bistable and where it is monostable in the absence of the RIFF. Therefore, in the presence of the RIFF, once the condition of the onset of oscillations in the rotating frame is met, $J_T q_{\text{st}} > 2\Gamma$, these oscillations are stabilized at the value of H_{RWA} given by $K \equiv K(H_{\text{RWA}}) = (2\Gamma/J_T q_{\text{st}}) < 1$. We emphasize that the frequency of these oscillations $2\pi/\mathbb{T}(H_{\text{RWA}})$ is small compared to ω_F , yet it exceeds Γ and $J_T q_{\text{st}}$.

The parameter $J_T q_{\text{st}}$ depends on the amplitude of the driving field F and the frequency ω_F . By varying F and ω_F one can control the stable value of H_{RWA} and thus the amplitude and frequency of the oscillations in the rotating frame. Remarkably, these oscillations become significantly nonsinusoidal already for comparatively small difference between H_{RWA} and its minimal value. This is seen in Fig. 1(b). The profoundly non-elliptical trajectories are a signature of nonsinusoidal vibrations. Formally, the oscillations are described by the Jacobi elliptic functions, which allows finding their Fourier components in the explicit form [34].

The instability of the forced vibrations at the drive frequency and the onset of nonlinear self-sustained oscillations in the rotating frame lead to a qualitative change of the power spectrum of the driven oscillator. The δ -shaped peak at the drive frequency ω_F disappears, and instead there emerge multiple equally spaced peaks on the both sides of ω_F that correspond to the vibration overtones in the rotating frame. The spacing between the peaks is small compared to ω_F . The widths of the peaks are determined by phase diffusion due to the noise in a nanoresonator, in particular, the thermal fluctuations of H_{RWA} around its stable value and the related fluctuations of the frequency $2\pi/\mathbb{T}(H_{\text{RWA}})$. These fluctuations are efficiently averaged out by the relaxation, the process reminiscent of motional narrowing in NMR [26, 35]. Therefore the widths of the peaks should be much smaller than the damping rate Γ . Such behavior has indeed been observed in the experiment [20].

In conclusion, we have shown that, from the symmetry and resonance arguments, a resonantly driven vibrational mode can experience a specific friction force. This force, the RIFF, is nonlinear in the mode coordinate and explicitly depends on the driving force. We considered a microscopic mechanism of the RIFF in nanomechanics associated with the driving-induced spatially nonuniform heating of a nanoresonator and the resulting change of the mode eigenfrequency. The RIFF can be negative. In this case, already for a moderately strong resonant drive, it can lead to an instability of forced vibrations of a weakly damped nonlinear mode, qualitatively modifying the familiar response of such a mode to a resonant drive. The instability causes the onset of self-sustained oscillations in the rotating frame. In turn, this leads to a characteristic structure of the power spectrum of the driven mode.

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Appendix A: Thermally induced nonlinear friction

Here we discuss the temperature change and the resulting change of the vibration eigenfrequency of a resonantly

driven nanomechanical resonator. In the units used in the main text, where we set the effective mass equal to unity, the displacement at the mode antinode has dimension $[q] = \text{g}^{1/2}\text{cm}$, whereas the resonant force has dimension $[F] = \text{g}^{1/2}\text{cm/s}^2$. If we consider a flexural mode in a quasi one-dimensional beam or a string, the displacement as a function of the coordinate x along the beam is $u(x, t) = \rho_{1D}^{-1/2}\phi(x)q(t)$, where ρ_{1D} is the density per unit length and $\phi(x)$ gives the shape of the mode, $\int \phi^2 dx = 1$. The energy in the driving field is $-\int dx f(x, t)u(x, t)$, where $f(x, t)$ is the “true” force per unit length. If we think of the force-induced term in the equation of motion as $[\rho_{1D}\ddot{u}(x)]_F = f(x, t)$, then we have for the force in the equation for q [Eq. (3) of the main text] the expression $F(t) = \rho_{1D}^{-1/2} \int dx f(x, t)\phi(x)$. Experiments on nanomechanical systems can be usually well described if one assumes that the force $f(x, t)$ can be factored into a space- and time-dependent parts, $f(x, t) = \tilde{f}_{\text{sp}}(x)f_t(t)$. Then

$$F(t) = \rho_{1D}^{-1/2} f_t(t) \int dx f_{\text{sp}}(x)\phi(x). \quad (\text{A1})$$

The power dissipated by the force per unit length is $f(x, t)\partial_t u(x, t)$. For a uniform isotropic resonator, the full equation for the increment of the temperature field is

$$C_r \partial_t \delta T = k_r \partial_x^2 \delta T + f(x, t) \partial_t u(x, t) / S, \quad (\text{A2})$$

where C_r is the specific heat of the resonator per unit volume, k_r is the thermal conductivity, and S is the cross-section area. We assume here that the temperature is constant across the resonator; an extension to a more general case, including the Zener thermoelastic relaxation [36] (see also [37]) is beyond the scope of this paper.

Equation (A2) has to be complemented by the boundary conditions. Often it is assumed that the temperature at the boundary of a nanoresonator is fixed by the support [22], a condition that applies if the support has a large mass and a high thermal conductivity, for example. Equation (A2) can be then solved by expanding $\delta T(x, t)$ in the orthogonal eigenmodes $T_n(x)$ of the temperature field in the absence of the drive,

$$(k_r/C_r)\partial_x^2 T_n = -\lambda_n T_n, \quad \int dx T_n(x)T_m(x) = \delta_{nm}$$

(the analysis can be easily extended to a more complicated geometry of the resonator and to more complicated boundary conditions than $T_n = 0$).

The major contribution to the temperature change comes from the mode $T_n(x)$ that has the form close to that of $f(x)\phi(x)$. It depends on the boundary conditions for the temperature field, the spatial structure of the displacement field of the mode $\phi(x)$, and also the coordinate dependence of the driving field.

For dielectric nanoresonators the thermal conductivity is comparatively low. At room temperature $k_r \sim$

$10^6 \text{ erg}/(\text{cm} \cdot \text{s} \cdot \text{K})$, and the specific heat is $C_r \sim 10^7 \text{ erg}/(\text{cm}^3 \cdot \text{K})$. Then for the resonator length $l_r \sim 10 \mu\text{m}$, the relaxation time of low-lying thermal modes is $\tau_T \sim C_r l_r^2 / k_r \sim 10^{-5} \text{ s}$. This time significantly exceeds the period (reciprocal frequency) of the vibrational modes, which is typically below $10^{-6} - 10^{-7} \text{ s}$. Then the temperature field averages out the oscillating terms in $f(x, t)\partial_t u(x, t)$ in Eq. (A2). At the same time, τ_T is typically much shorter than the relaxation times of low-lying vibrational modes, which often exceeds the vibration period by a factor $> 10^4$. In this important case the temperature adiabatically follows the vibration amplitude.

The driving-induced temperature change is then of the form $\delta T(x, t) = \sum c_n(t)T_n(x)$ with

$$c_n = \rho_{1D}^{-1/2} (SC_r)^{-1} \lambda_n^{-1} \int dx T_n(x)\phi(x)[f(x, t)\dot{q}]_{\text{av}}, \quad (\text{A3})$$

where $[\dots]_{\text{av}}$ indicates averaging over the vibration period. For low-lying vibrational modes and for a weakly nonuniform driving force $f(x, t)$ the major contribution to $\delta T(x, t)$ comes from low-lying temperature modes, with $\lambda_n \sim 1/\tau_T$. Then the magnitude of the temperature change averaged over the resonator is

$$\delta T \sim l_r^2 k_r^{-1} S^{-1} [F(t)\dot{q}(t)]_{\text{av}}.$$

We note that the assumption of the temperature being constant in the resonator cross-section requires that $C_r l_{\perp}^2 / k_r$ (l_{\perp} is the typical transverse dimension) be much shorter than the vibration period, the condition well satisfied for the typical $l_{\perp} \lesssim 0.1 \mu\text{m}$.

The temperature change causes a change of the vibration frequency. There are several mechanisms of this effect [11]. One of them is the coupling of the mode to the phonons in the nanoresonator that is nonlinear in the mode strain. This coupling is fairly general. It emerges already from the combination of the standard cubic coupling of the considered low-frequency mode (in particular, a flexural mode) to acoustic phonons and the geometric nonlinearity, but it also comes from other terms in the nonlinear Hamiltonian of the vibrations in the resonator.

Phenomenologically, the mechanism can be described by taking into account the term in the free energy density of the nanoresonator $\delta \mathcal{F}$, which is quadratic in the linear strain tensor $\hat{\epsilon}(\mathbf{r})$ and linear in the temperature change $\delta T(\mathbf{r})$. A simplified form of this term in the one-dimensional model for a flexural mode is

$$\delta \mathcal{F} = -\gamma_{\mathcal{F}} \int dx \delta T(x) (\partial_x^2 u)^2, \quad (\text{A4})$$

where $\gamma_{\mathcal{F}}$ is the coupling constant; it is determined by the thermal expansion coefficient, the specific heat, and the resonator geometry [11]. The elastic part of the free energy in the harmonic approximation can be written as $\mathcal{F}_E = \frac{1}{2} \gamma_{\omega} \int dx [\partial_x^2 u]^2$ with γ_{ω} determined in the standard way by the elasticity and the geometry [38]; this

term gives the vibration frequency ω_0 for constant tem-

perature. It corresponds to the potential energy of the mode written as $\omega_0^2 q^2/2$.

Then the change of the vibration frequency due to the temperature change is

$$\delta\omega_0 = -(\omega_0\rho_{1D})^{-1}\gamma_{\mathcal{F}} \int dx \delta T(x)(\partial_x^2\phi)^2. \quad (\text{A5})$$

From Eqs. (A1), (A3), and (A5) we find that, for a slow thermal relaxation, the resonant driving induced force in the equation for $q(t)$ is

$$f_T = G_T [F(t)\dot{q}(t)]_{\text{av}} q(t), \quad G_T = 2\gamma_{\mathcal{F}}(\rho_{1D}SC_r)^{-1} \sum_n \lambda_n^{-1} \int dx T_n(x)\phi(x)f_{\text{sp}}(x) \\ \times \int dy T_n(y)(\partial_y^2\phi)^2 \left[\int dx f_{\text{sp}}(x)\phi(x) \right]^{-1}. \quad (\text{A6})$$

The coefficient G_T gives the coefficient $2m\omega_0\lambda_\omega\lambda_T$ in Eq. (2) of the main text, with the account taken of the spatial dependence of the temperature change.

It should be noted that the coupling (A4) also leads to the standard nonlinear friction, with the friction force that corresponds to $q^2\dot{q}$ or \dot{q}^3 in the phenomenological picture [11]. However, in the considered case of slow thermal relaxation this force has an extra factor $\propto (\tau_T\omega_0)^{-2}$. Therefore it can be small compared to the force f_T .

In prestressed nanoresonators, an important mecha-

nism of the coupling of the frequency and temperature changes is related to the change of the tension due to thermal expansion, cf. [22] and references therein. It can be analyzed in a way similar to that described above and leads to a qualitatively similar result. If the thermal expansion coefficient is positive, this mechanism leads to the decrease of the vibration frequency with an increasing drive strength, as does the geometric nonlinearity.

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